Tokyo 2015 - JBC Local Flow Analysis

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JBC local flow analysis 1/3

- This analysis is very preliminary and has been written in the urgency under high pressure,
- For the JBC, the proceedings composed of more than 1000 pages and 6000 figures were sent only 5 days ago...
- The objectives of this discussion are to assess the current CFD simulations, identify limitations and to some extent provide guidelines for future research directions.
- This workshop gives an opportunity of exchanges in order to progress towards even better simulation practices in marine hydrodynamics.

More specifically, we will see if:

- The main characteristics of the flow around the naked JBC hull are captured and by which combination of grids and turbulence models,
- The influence of the duct on the flow without propeller is correctly predicted,
- The influence of propeller on the flow around the naked hull is also correctly predicted,
- The influence of the duct on the flow around the hull with propeller is reliaby simulated and leads to a reduction of the energy consumption.

JBC local flow analysis 3/3

Five configurations should be analyzed from a local flow standpoint

- Case 1-3a (Re=7.46 10⁶, Fr=0.142, without duct, without propeller, (Experiments from NMRI)
- Case 1-3b (Re=2.74 10⁶, Fr=0.0, without duct, without propeller, (Wind tunnel experiments from TUHH)
- Case 1-4 (Re=7.46 10⁶, Fr=0.142, with duct, without propeller, (Experiments from NMRI)
- Case 1-7 (Re=7.46 10⁶, Fr=0.142, without duct, with propeller, (Experiments from NMRI)
- Case 1-8 (Re=7.46 10⁶, Fr=0.142, with duct, with propeller, (Experiments from NMRI)

In all the test cases, the rudder is omitted.

The analysis will be performed on the basis of the proceedings for all the cases and an additional local vortex flow analysis will be presented for case 1-3a.





JBC - Case 1-3a



Iso-U contours - Station S2



Cross-flow velocity components - Station S2



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Iso-U contours - Station S4



Cross-flow velocity components - Station S4



Iso-U contours - Station S7



Cross-flow velocity components - Station S7



Grid sensitivity

Grids can be organized into three groups for 18 participants:

- Not So Fine: Ncell < 2 M cells (MARIC, HHI)
- Fine: 2 M cells < Ncell < 10 M cells (ABS, CHALMERS, INSEAN, ECN, HSVA, KRISO, SHIME, NMRI, PNU, YNU, CSSR)
- Very Fine: 10 M cells < Ncell < 50 M cells (SOTON, MHI, MARIN, URO)
- Tremendously Fine: Ncell > 50 M cells (None)

Comparison with Gothenburg 2010 (average size was 4M cells) Just a global picture: one does not have access to the local grid density !

Grid influence - Station S2 - Grid comparison from SHIME



Grid influence - Station S4 - Grid comparison from SHIME



Grid influence - Station S7 - Grid comparison from SHIME



Grid influence - Station S2



Similar turbulence model (k- ω sst) but different grid category

Grid influence - Station S4



Grid influence - Station S7



Influence of the Turbulence Closures

Turbulence models can be organized into three groups:

- The isotropic linear closures: INSEAN (Spalart-Allmaras), HSVA (Linear EASM), MARIN (k-w SST + DM), MARIC (k-w SST), URO (k-w SST), PNU (k-e), SHIME (k-w SST), CSSRC (k-e), ABS (k-w SST), SOTON (k-w SST), ECN-CNRS ((k-w SST),MHI (k-w SST),
- The anisotropic non-linear models: MHI (RSM), ECN-CNRS (EASM), NMRI (EASM), CHALMERS (EASM), YNU (EASM), KRISO (EASM)
- The hybrid LES models: URO (Hybrid).

Linear Isotropic Turbulence Closures

Linear Isotropic Turbulence Closures - Station S2



Linear Isotropic Turbulence Closures - Station S4



Linear Isotropic Turbulence Closures - Station S7











Non-Linear Anisotropic Turbulence Closures

Isotropic vs Anisotropic turbulence closures - Station S2



Isotropic vs Anisotropic turbulence closures - Station S4



Isotropic vs Anisotropic turbulence closures - Station S7




EASM Turbulence Closures - Station S2



EASM Turbulence Closures - Station S4



EASM Turbulence Closures - Station S7



Full RSM Transport Turbulence Closures

Full RSM Transport Turbulence Closures - Station S2



Full RSM Transport Turbulence Closures - Station S4



Full RSM Transport Turbulence Closures - Station S7



Hybrid LES Turbulence Closures













Influence of the free-surface

Influence of the free-surface - Station S2



Influence of the free-surface - Station S4



Influence of the free-surface - Station S7



Influence of the wall boundary condition

Influence of the wall boundary condition - Station S2



Influence of the wall boundary condition - Station S4



Influence of the wall boundary condition - Station S7



Codes comparison

Code comparison - Station S2



Same grid, same turbulence model

Code comparison - Station S4



Same grid, same turbulence model

Code comparison - Station S7



Same grid, same turbulence model

Case 1-3a - Temporary conclusions 1/2

- With the typical grids used (5-10 M points), the influence from the grid discretisation is moderate for RANSE,
- The major influence comes from the turbulence closure. Linear isotropic closures under-predict the longitudinal vorticity at S2 while full RSM closures slightly over-predict it at the same station.
- Non-linear anisotropic closures offer a good compromise from the standpoint of the local flow although they slightly underpredict the vorticity at S2.
- New results from hybrid LES are promising but IDDES seems to over-predict the vorticity again (need to check TKE in the bilge vortex).

- Codes seem to be mature since we do not observe large discrepancies when same turbulence closures on similar grids are used.
- The infuence of the free-surface on the local flow is not negligible.
- The infuence of the wall boundary condition on the local flow is weak.

JBC - Case 1-3a Local vortex flow analysis

Objectives of this local analysis

- Previously, the local flow analysis was uniquely based on the inspection of the flow characteristics at specific cross-sections where experiments were available.
- This typical assessment provides a global picture of the flow for each experimental cross-section. This interpretation can be misleading since it is based on visual inspection.
- Here, we would like to enrich this cross-section based evaluation by a more detailed and local vortex flow analysis in order to draw more elaborate conclusions about the generation and evolution of the longitudinal vortices.

- Longitudinal evolution of characteristic flow data in the core of the main vortex (by drawing a streamline through the center of the vortex at station S4),
- Y and Z transversal evolutions of characteristic flow data across the vortex center at stations S2, S4 and S7.

Difficulties and perils of the exercise

The longitudinal and transversal evolutions in the vortex core

- It was first decided to use the same information in computations and experiments to locate the vortex center,
- Since we have no volumic information from the measurements (no tomographic PIV), we were forced to use the local $max(\omega_x)$ to locate the vortex center in each section instead of max(Q),
- The procedure is more or less OK for stations S4 an S7 where the main vortex is roughly aligned with X but it is less justified for station S2 where (for some computations), the vortex is not aligned with X.
- Therefore, additional figures were produced based on max(Q) instead of max(ω_x) to locate the center of the vortex at station S2.

JBC - Case 1-3a Local vortex flow analysis

Genesis from NATO-AVT183 DTMB5415 at straight ahead condition

NATO AVT183 - DTMB5415 at straight ahead condition



3D view (SDV and FBKV vortices)



IIHR 3D experiments (ω_x) behind the sonar dome

DTMB 5415 - SDV core longitudinal evolution



DTMB 5415 - SDV radial evolution



 ω_x





Invariant Q





-0.002

0.000

Radial Location TKE

0.0025

0.002

0.001

0.0005

-0.006

-0.004

₩0.0015

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0.007

0.004

0.006

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JBC - Case 1-3a Local vortex flow analysis Longitudinal evolution













JBC - Case 1-3a Local vortex flow analysis Transversal evolution







 ω_x



 ω_x







TKE



TKE







 ω_x



 ω_x







TKE



TKE







 ω_x



 ω_x







TKE



TKE

TKE distribution at station S2 (Hybrid LES from URO)



Total TKE

Resolved TKE

TKE distribution at station S4 (Hybrid LES from URO)



Total TKE

Resolved TKE

TKE distribution at station S7 (Hybrid LES from URO)



Total TKE

Resolved TKE

Temporary conclusions 1/2

- Relative dispersion of the computations,
- Lack of grid points to assess the flow characterisitics in the core,
- Lack of experimental points to trust the measurements,
- Few expected transverse evolutions of quantities like Q or ω_x,
- Influence of the turbulence closures reinforced by this local analysis,
- To be continued with locally refined experimental and computational grids,
- Important to use 3D tomographic PIV to trust this analysis, whatever the vortex evolution.
- Non-linear anisotropic closures increase the maximum vorticity (and Q) in the core,
- Hybrid LES closure from URO is the only one able to predict the right level of TKE,
- In this case, the major part of TKE comes from the computed contribution.

JBC - Case 1-3b



Re=2.74 10⁶, Fr=0. Experiments from TUHH

JBC - Case 1-3b



Iso-U contours - Station S2



Iso-U contours - Station S4



Iso-U contours - Station S7



Grids can be classified into 3 groups for 3 participants:

- Not So Fine: Ncell < 2 M cells (None)</p>
- Fine: 2 M cells < Ncell < 10 M cells (ECN without AGR)
- Very Fine: 10 M cells < Ncell < 50 M cells (ECN with AGR)
- Tremendously Fine: Ncell > 50 M cells (FOI (150M cells), SRC (4.9G cells !!!))

Comparison with Gothenburg 2010 (average size was 4M cells) Just a global picture: one does not have access to the local grid density ! **Grid influence**



Automatic Grid Refinement (AGR) is controled by the Hessian of the velocity flux



Automatic Grid Refinement (AGR) is controled by the Hessian of the velocity flux



Automatic Grid Refinement (AGR) is controled by the Hessian of the velocity flux



Points are added in the regions of high shear stress



Points are added in the regions of high shear stress



Points are added in the regions of high shear stress

Turbulence models can be organized into three groups:

- The isotropic linear closures: FOI (k-ω SST),
- The anisotropic non-linear models: ECN-CNRS (EASM),
- The LES models: FOI (NWM-LES), SRC (LES).

Linear Isotropic Turbulence Closures

Linear Isotropic Turbulence Closures - Station S2



Linear Isotropic Turbulence Closures - Station S4



Linear Isotropic Turbulence Closures - Station S7



Non-Linear Anisotropic Turbulence Closures

Non-Linear Anisotropic Turbulence Closures - Station S2



Non-Linear Anisotropic Turbulence Closures - Station S4



Non-Linear Anisotropic Turbulence Closures - Station S7



LES Turbulence Closures













TKE contours - Station S2



TKE contours - Station S4



TKE contours - Station S7





ECN-CNRS/EASM Max TKE 0.018 SRC/LES Max TKE 0.024

Case 1-3b - Temporary conclusions

- A sensitivity to the local grid density is observed, which contradicts somewhat the conclusions drawn for the previous case,
- The major influence comes from the turbulence closure. Linear isotropic closures under-predict the longitudinal vorticity at S2 while full RSM closures tend to over-predict it at the same station.
- For the first time, two LES computations are presented.
- LES results from SRC predict the right level of TKE in the core of the bilge vortex (higher than what is modeled by EASM)
- Results from NWM-LES are promising but this model seems to over-predict the vorticity (need to check TKE in the bilge vortex)





Experiments from NMRI

JBC - Case 1-4



Experiments from NMRI
Influence of the duct - Experiments















Linear Isotropic Turbulence Closures

























Non-Linear Anisotropic Turbulence Closures

Isotropic vs Anisotropic turbulence closures - Station S2



Isotropic vs Anisotropic turbulence closures - Station S4



Isotropic vs Anisotropic turbulence closures - Station S7





















Full RSM Transport Turbulence Closures

Full RSM Transport Turbulence Closures - Station S2



Full RSM Transport Turbulence Closures - Station S4


Full RSM Transport Turbulence Closures - Station S7



JBC - Case 1-7 Without duct, with propeller

Influence of the propeller - Experiments

Propeller influence - Station S2



Propeller influence - Station S2



Station S4 - 0 deg.



Station S4 - 24 deg.



Station S4 - 48 deg.



Station S7 - 0 deg.



Station S7 - 24 deg.



Station S7 - 48 deg.



Comparison of results

Linear Isotropic Turbulence Closures - Station S4 - 0 deg.



Linear Isotropic Turbulence Closures - Station S4 - 24 deg.



Linear Isotropic Turbulence Closures - Station S4 - 48 deg.



Linear Isotropic Turbulence Closures - Station S2



Linear Isotropic Turbulence Closures - Station S4 - 0 deg.



Linear Isotropic Turbulence Closures - Station S4 - 24 deg.



Linear Isotropic Turbulence Closures - Station S4 - 48 deg.



JBC - Case 1-8 With duct, with propeller

Influence of the duct - Experiments

Duct influence - Station S2



Duct influence - Station S4 - 0 deg.



Duct influence - Station S4 - 24 deg.



Duct influence - Station S4 - 48 deg.



Duct influence - Station S4 - Temporal mean



Duct influence - Station S7 - 0 deg.



Duct influence - Station S7 - 24 deg.



Duct influence - Station S7 - 48 deg.



Duct influence - Station S7 - Temporal mean



It is 2:00 am today and this is the end of this presentation... Thank you for your understanding !